

LM1085 3-A Low Dropout Positive Regulators

1 Features

- Available in 3.3-V, 5.0-V, 12-V and Adjustable Versions
- Current Limiting and Thermal Protection
- Output Current 3 A
- Line Regulation 0.015% (typical)
- Load Regulation 0.1% (typical)

2 Applications

- High Efficiency Linear Regulators
- Battery Charger
- Post Regulation for Switching Supplies
- Constant Current Regulator
- Microprocessor Supply

3 Description

The LM1085 is a regulator with a maximum dropout of 1.5 V at 3 A of load current. It has the same pin-out as TI's industry standard LM317.

Two resistors are required to set the output voltage of the adjustable output voltage version of the LM1085. Fixed output voltage versions integrate the adjust resistors.

The LM1085 circuit includes a zener trimmed bandgap reference, current limiting and thermal shutdown.

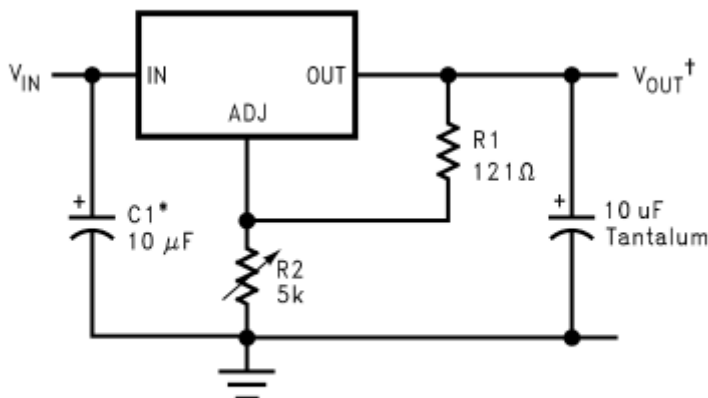
Refer to the LM1084 for the 5A version, and the LM1086 for the 1.5A version.

Device Information⁽¹⁾

PART NUMBER	PACKAGE	BODY SIZE (NOM)
LM1085	DDPAK/TO-263 (3)	10.18 mm × 8.41 mm
	TO-220 (3)	14.986 mm × 10.16 mm

(1) For all available packages, see the orderable addendum at the end of the datasheet.

Typical Application



*NEEDED IF DEVICE IS FAR FROM FILTER CAPACITORS

$${}^{\dagger}V_{\text{OUT}} = 1.25\text{V} \left(1 + \frac{R2}{R1}\right)$$

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) ⁽¹⁾⁽²⁾

	MIN	MAX	UNIT
Maximum Input to Output Voltage Differential			
LM1085-ADJ		29	V
LM1085-12		18	V
LM1085-3.3		27	V
LM1085-5.0		25	V
Power Dissipation ⁽³⁾		Internally Limited	V
Junction Temperature (T _J) ⁽⁴⁾		150	°C
Lead Temperature		260, to 10 sec	°C
Storage temperature range, T _{stg}	-65	150	°C

- (1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/ Distributors for availability and specifications.
- (3) Power dissipation is kept in a safe range by current limiting circuitry. Refer to *Overload Recovery*.
- (4) The maximum power dissipation is a function of T_{J(max)}, θ_{JA}, and T_A. The maximum allowable power dissipation at any ambient temperature is P_D = (T_{J(max)} - T_A) / θ_{JA}. All numbers apply for packages soldered directly into a PC board. Refer to Thermal Considerations in the Application Notes.

6.2 ESD Ratings

	VALUE	UNIT
V _(ESD) Electrostatic discharge Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	V

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

	MIN	MAX	UNIT
Junction Temperature (T _J) ⁽¹⁾	-40	125	°C

- (1) The maximum power dissipation is a function of T_{J(max)}, θ_{JA}, and T_A. The maximum allowable power dissipation at any ambient temperature is P_D = (T_{J(max)} - T_A) / θ_{JA}. All numbers apply for packages soldered directly into a PC board. Refer to Thermal Considerations in the Application Notes.

6.4 Thermal Information

THERMAL METRIC ⁽¹⁾	LM1085		UNIT
	KTT	NDE	
	3 PINS	3 PINS	
R _{θJA} Junction-to-ambient thermal resistance	40.6	22.8	°C/W
R _{θJC(top)} Junction-to-case (top) thermal resistance	43.0	15.6	
R _{θJB} Junction-to-board thermal resistance	23.1	4.2	
ψ _{JT} Junction-to-top characterization parameter	9.9	2.2	
ψ _{JB} Junction-to-board characterization parameter	22.1	4.2	
R _{θJC(bot)} Junction-to-case (bottom) thermal resistance	0.7	0.7	

- (1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](#).

6.5 Electrical Characteristics

Minimum and Maximum limits are ensured through test, design, or statistical correlation. Typical values represent the most likely parametric norm at $T_J = 25^\circ\text{C}$, and are provided for reference purposes only.

PARAMETER		TEST CONDITIONS	MIN ⁽¹⁾	TYP ⁽²⁾	MAX ⁽¹⁾	UNIT
V_{REF}	Reference Voltage ⁽³⁾	LM1085-ADJ, $I_{OUT} = 10\text{ mA}$, $V_{IN} - V_{OUT} = 3\text{ V}$, $10\text{ mA} \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $1.5\text{ V} \leq (V_{IN} - V_{OUT}) \leq 15\text{ V}$	1.238	1.250	1.262	V
		LM1085-ADJ, $I_{OUT} = 10\text{ mA}$, $V_{IN} - V_{OUT} = 3\text{ V}$, $10\text{ mA} \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $1.5\text{ V} \leq (V_{IN} - V_{OUT}) \leq 15\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	1.225	1.250	1.270	
V_{OUT}	Output Voltage ⁽³⁾	LM1085-3.3, $I_{OUT} = 0\text{ mA}$, $V_{IN} = 5\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $4.8\text{ V} \leq V_{IN} \leq 15\text{ V}$	3.270	3.300	3.330	V
		LM1085-3.3, $I_{OUT} = 0\text{ mA}$, $V_{IN} = 5\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $4.8\text{ V} \leq V_{IN} \leq 15\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	3.235	3.300	3.365	V
		LM1085-5.0, $I_{OUT} = 0\text{ mA}$, $V_{IN} = 8\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $6.5\text{ V} \leq V_{IN} \leq 20\text{ V}$	4.950	5.000	5.050	V
		LM1085-5.0, $I_{OUT} = 0\text{ mA}$, $V_{IN} = 8\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $6.5\text{ V} \leq V_{IN} \leq 20\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	4.900	5.000	5.100	V
		LM1085-12, $I_{OUT} = 0\text{ mA}$, $V_{IN} = 15\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $13.5\text{ V} \leq V_{IN} \leq 25\text{ V}$	11.880	12.000	12.120	V
		LM1085-12, $I_{OUT} = 0\text{ mA}$, $V_{IN} = 15\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $13.5\text{ V} \leq V_{IN} \leq 25\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	11.760	12.000	12.240	V
ΔV_{OUT}	Line Regulation ⁽⁴⁾	LM1085-ADJ, $I_{OUT} = 10\text{ mA}$, $1.5\text{ V} \leq (V_{IN} - V_{OUT}) \leq 15\text{ V}$		0.015	0.2	mV
		LM1085-ADJ, $I_{OUT} = 10\text{ mA}$, $1.5\text{ V} \leq (V_{IN} - V_{OUT}) \leq 15\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		0.035	0.2	
		LM1085-3.3, $I_{OUT} = 0\text{ mA}$, $4.8\text{ V} \leq V_{IN} \leq 15\text{ V}$		0.5	6	mV
		LM1085-3.3, $I_{OUT} = 0\text{ mA}$, $4.8\text{ V} \leq V_{IN} \leq 15\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		1.0	6	
		LM1085-5.0, $I_{OUT} = 0\text{ mA}$, $6.5\text{ V} \leq V_{IN} \leq 20\text{ V}$		0.5	10	mV
		LM1085-5.0, $I_{OUT} = 0\text{ mA}$, $6.5\text{ V} \leq V_{IN} \leq 20\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		1.0	10	
		LM1085-12, $I_{OUT} = 0\text{ mA}$, $13.5\text{ V} \leq V_{IN} \leq 25\text{ V}$		1.0	25	mV
		LM1085-12, $I_{OUT} = 0\text{ mA}$, $13.5\text{ V} \leq V_{IN} \leq 25\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		2.0	25	
ΔV_{OUT}	Load Regulation ⁽⁴⁾	LM1085-ADJ, $(V_{IN} - V_{OUT}) = 3\text{ V}$, $10\text{ mA} \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$		0.1	0.3	mV
		LM1085-ADJ, $(V_{IN} - V_{OUT}) = 3\text{ V}$, $10\text{ mA} \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		0.2	0.4	
		LM1085-3.3, $V_{IN} = 5\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$		3	15	mV
		LM1085-3.3, $V_{IN} = 5\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		7	20	
		LM1085-5.0, $V_{IN} = 8\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$		5	20	mV
		LM1085-5.0, $V_{IN} = 8\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		10	35	
		LM1085-12, $V_{IN} = 15\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$		12	36	mV
		LM1085-12, $V_{IN} = 15\text{ V}$, $0 \leq I_{OUT} \leq I_{FULL\text{ LOAD}}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		24	72	
V_{DO}	Dropout Voltage ⁽⁵⁾	LM1085-ADJ, 3.3, 5, 12, ΔV_{REF} , $\Delta V_{OUT} = 1\%$, $I_{OUT} = 3\text{ A}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		1.3	1.5	V

(1) All limits are specified by testing or statistical analysis.

(2) Typical Values represent the most likely parametric norm.

(3) $I_{FULL\text{ LOAD}}$ is defined in the current limit curves. The $I_{FULL\text{ LOAD}}$ Curve defines the current limit as a function of input-to-output voltage. Note that 30W power dissipation for the LM1085 is only achievable over a limited range of input-to-output voltage.

(4) Load and line regulation are measured at constant junction temperature, and are ensured up to the maximum power dissipation of 30W. Power dissipation is determined by the input/output differential and the output current. Ensured maximum power dissipation will not be available over the full input/output range.

(5) Dropout voltage is specified over the full output current range of the device.

Electrical Characteristics (continued)

Minimum and Maximum limits are ensured through test, design, or statistical correlation. Typical values represent the most likely parametric norm at $T_J = 25^\circ\text{C}$, and are provided for reference purposes only.

PARAMETER		TEST CONDITIONS	MIN ⁽¹⁾	TYP ⁽²⁾	MAX ⁽¹⁾	UNIT
I_{LIMIT}	Current Limit	LM1085-ADJ, $V_{IN}-V_{OUT} = 5\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	3.2	5.5		A
		LM1085-ADJ, $V_{IN}-V_{OUT} = 25\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	0.2	0.5		
		LM1085-3.3, $V_{IN} = 8.0\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	3.2	5.5		A
		LM1085-5.0, $V_{IN} = 10\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	3.2	5.5		A
		LM1085-12, $V_{IN} = 17\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	3.2	5.5		A
	Minimum Load Current ⁽⁶⁾	LM1085-ADJ, $V_{IN}-V_{OUT} = 25\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		5.0	10.0	mA
I_{GND}	Quiescent Current	LM1085-3.3, $V_{IN} \leq 18\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		5.0	10.0	mA
		LM1085-5.0, $V_{IN} \leq 20\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		5.0	10.0	mA
		LM1085-12, $V_{IN} \leq 25\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		5.0	10.0	mA
	Thermal Regulation	$T_A = 25^\circ\text{C}$, 30ms Pulse		.004	0.02	%/W
	Ripple Rejection	$f_{RIPPLE} = 120\text{Hz}$, $C_{OUT} = 25\mu\text{F}$ Tantalum, $I_{OUT} = 3\text{A}$, LM1085-ADJ, $C_{ADJ} = 25\mu\text{F}$, $(V_{IN}-V_O) = 3\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	60	75		dB
		LM1085-3.3, $V_{IN} = 6.3\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	60	72		dB
		LM1085-5.0, $V_{IN} = 8.0\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	60	68		dB
		LM1085-12, $V_{IN} = 15\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$	54	60		dB
I_{ADJ}	Adjust Pin Current	LM1085-ADJ		55		μA
		LM1085-ADJ, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$			120	
ΔI_{ADJ}	Adjust Pin Current Change	LM1085-ADJ, $10\text{mA} \leq I_{OUT} \leq I_{FULL\ LOAD}$, $1.5\text{ V} \leq V_{IN}-V_{OUT} \leq 25\text{ V}$, $-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		0.2	5	μA
	Temperature Stability	$-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$		0.5		
	Long Term Stability	$T_A = 125^\circ\text{C}$, 1000 Hrs		0.3	1.0	
	RMS Output Noise (% of V_{OUT})	$10\text{Hz} \leq f \leq 10\text{ kHz}$		0.003		

(6) The minimum output current required to maintain regulation.

6.6 Typical Characteristics

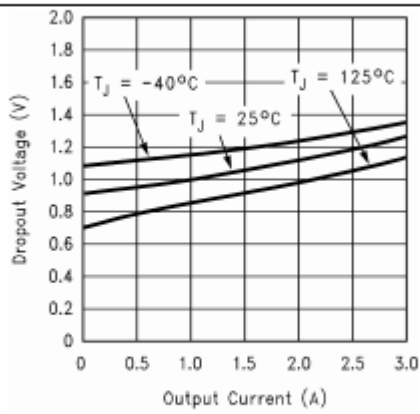


Figure 1. Dropout Voltage vs Output Current

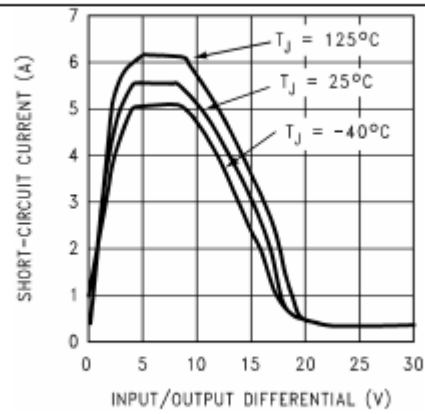


Figure 2. Short-Circuit Current vs Input/Output Difference

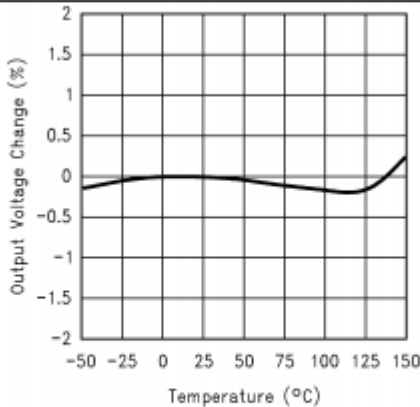


Figure 3. Percent Change in Output Voltage vs Temperature

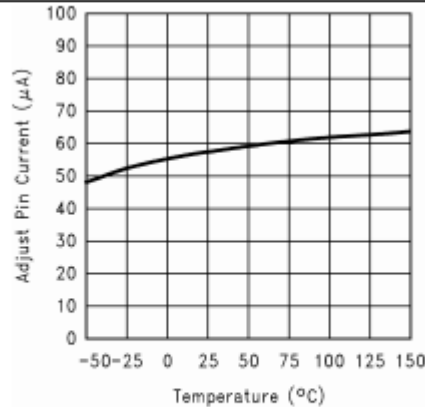


Figure 4. Adjust Pin Current vs Temperature

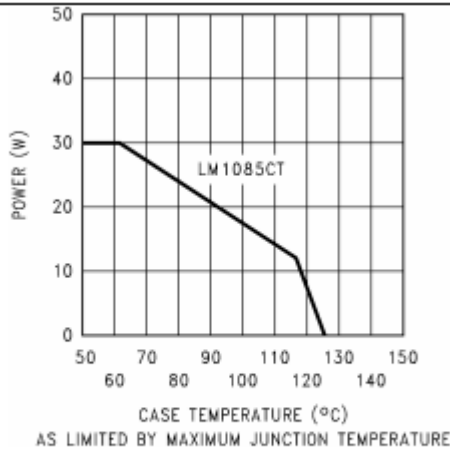


Figure 5. Maximum Power Dissipation vs Temperature

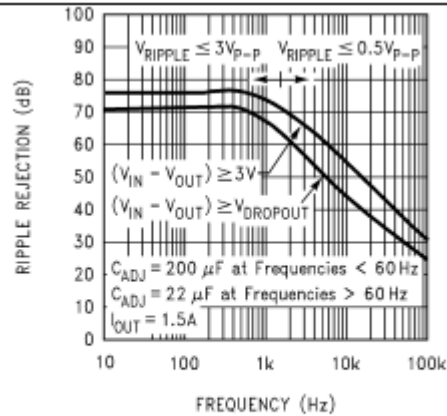


Figure 6. Ripple Rejection vs Frequency (LM1085-Adj.)

Typical Characteristics (continued)

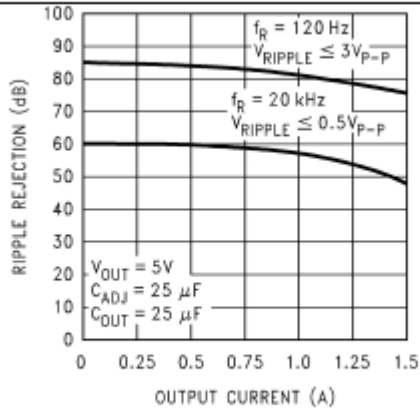


Figure 7. Ripple Rejection vs Output Current (LM1085-ADJ)

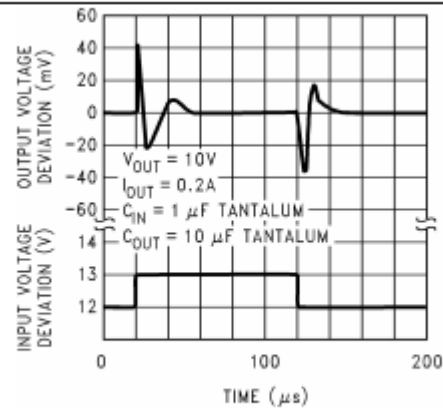


Figure 8. Line Transient Response

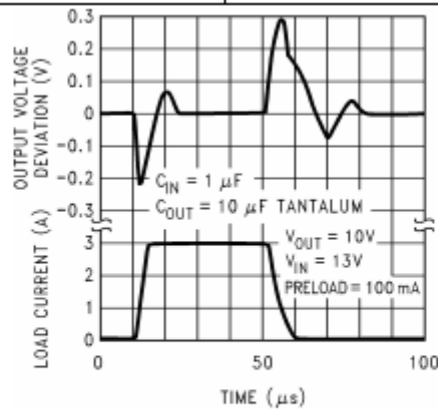


Figure 9. Load Transient Response

7 Detailed Description

7.1 Overview

A basic functional diagram for the LM1085-ADJ (excluding protection circuitry) is shown in Figure 10. The topology is basically that of the LM317 except for the pass transistor. Instead of a Darlington NPN with its two diode voltage drop, the LM1085 uses a single NPN. This results in a lower dropout voltage. The structure of the pass transistor is also known as a quasi LDO. The advantage of a quasi LDO over a PNP LDO is its inherently lower quiescent current. The LM1085 is ensured to provide a minimum dropout voltage of 1.5V over temperature, at full load.

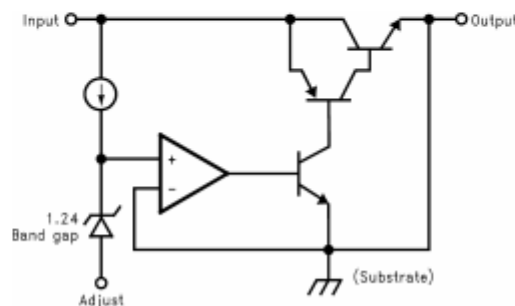
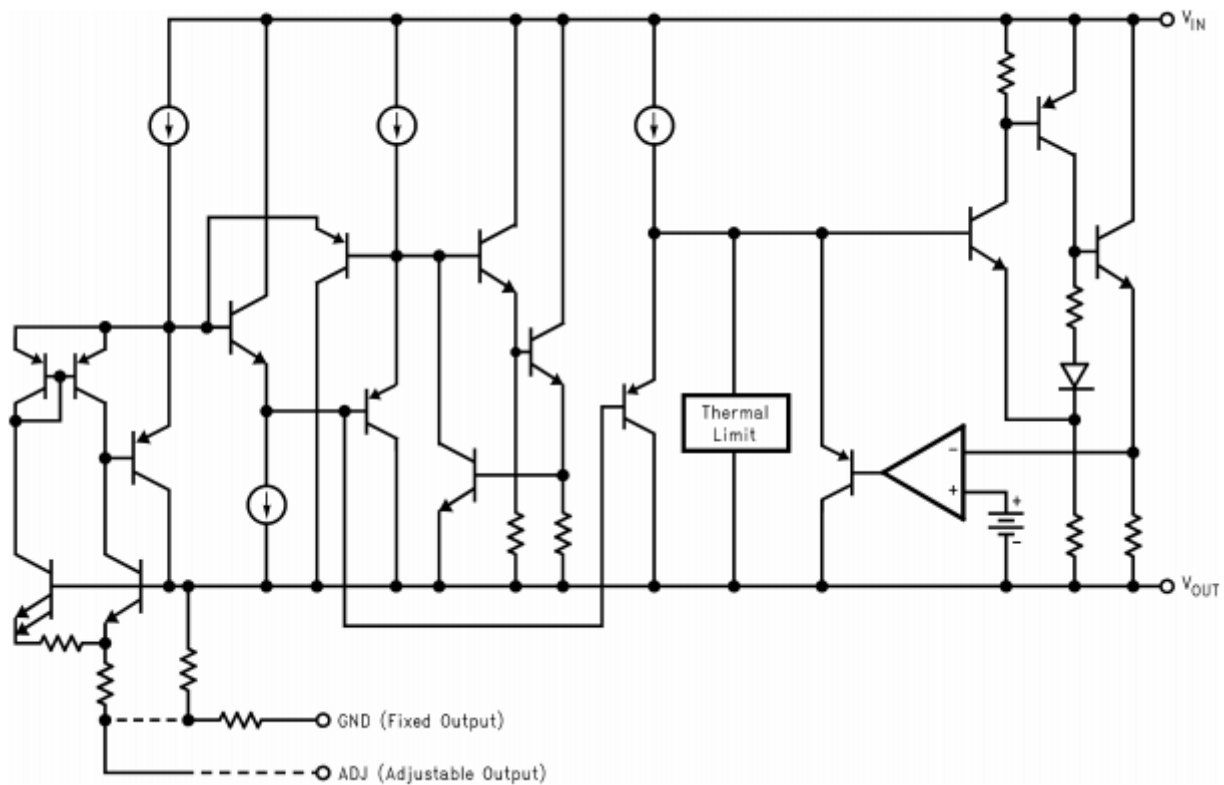


Figure 10. Basic Functional Diagram for the LM1085, Excluding Protection Circuitry

7.2 Functional Block Diagram



7.3 Feature Description

7.3.1 Ripple Rejection

Ripple rejection is a function of the open loop gain within the feed-back loop (refer to and [Figure 13](#)). The LM1085 exhibits 75dB of ripple rejection (typ.). When adjusted for voltages higher than V_{REF} , the ripple rejection decreases as function of adjustment gain: $(1+R1/R2)$ or V_O/V_{REF} . Therefore a 5V adjustment decreases ripple rejection by a factor of four (-12dB); Output ripple increases as adjustment voltage increases.

However, the adjustable version allows this degradation of ripple rejection to be compensated. The adjust terminal can be bypassed to ground with a capacitor (C_{ADJ}). The impedance of the C_{ADJ} should be equal to or less than $R1$ at the desired ripple frequency. This bypass capacitor prevents ripple from being amplified as the output voltage is increased.

$$1/(2\pi \cdot f_{RIPPLE} \cdot C_{ADJ}) \leq R_1 \quad (1)$$

7.3.2 Load Regulation

The LM1085 regulates the voltage that appears between its output and ground pins, or between its output and adjust pins. In some cases, line resistances can introduce errors to the voltage across the load. To obtain the best load regulation, a few precautions are needed.

Figure 11 shows a typical application using a fixed output regulator. R_{t1} and R_{t2} are the line resistances. V_{LOAD} is less than the V_{OUT} by the sum of the voltage drops along the line resistances. In this case, the load regulation seen at the R_{LOAD} would be degraded from the data sheet specification. To improve this, the load should be tied directly to the output terminal on the positive side and directly tied to the ground terminal on the negative side.

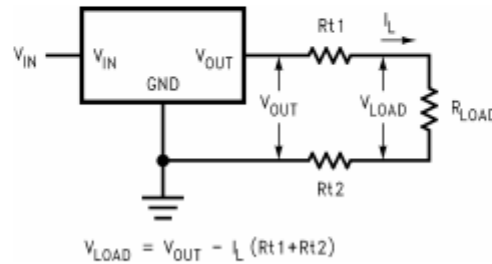


Figure 11. Typical Application Using Fixed Output Regulator

When the adjustable regulator is used (Figure 12), the best performance is obtained with the positive side of the resistor R_1 tied directly to the output terminal of the regulator rather than near the load. This eliminates line drops from appearing effectively in series with the reference and degrading regulation. For example, a 5V regulator with 0.05Ω resistance between the regulator and load will have a load regulation due to line resistance of $0.05\Omega \times I_L$. If $R_1 (= 125\Omega)$ is connected near the load the effective line resistance will be $0.05\Omega (1 + R_2/R_1)$ or in this case, it is 4 times worse. In addition, the ground side of the resistor R_2 can be returned near the ground of the load to provide remote ground sensing and improve load regulation.

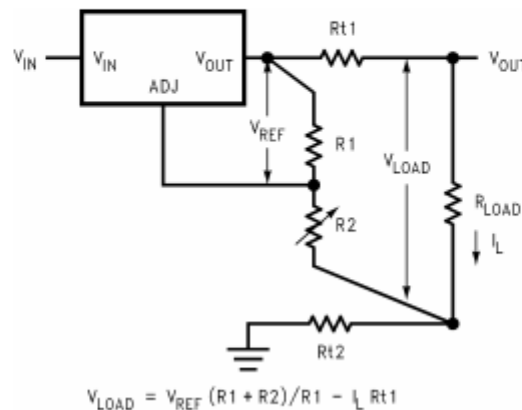


Figure 12. Best Load Regulation Using Adjustable Output Regulator

7.3.3 Overload Recovery

Overload recovery refers to regulator's ability to recover from a short circuited output. A key factor in the recovery process is the current limiting used to protect the output from drawing too much power. The current limiting circuit reduces the output current as the input to output differential increases. Refer to short circuit curve in the [Typical Characteristics](#) section.

During normal start-up, the input to output differential is small since the output follows the input. But, if the output is shorted, then the recovery involves a large input to output differential. Sometimes during this condition the current limiting circuit is slow in recovering. If the limited current is too low to develop a voltage at the output, the voltage will stabilize at a lower level. Under these conditions it may be necessary to recycle the power of the regulator in order to get the smaller differential voltage and thus adequate start up conditions. Refer to [Typical Characteristics](#) section for the short circuit current vs. input differential voltage.

7.4 Device Functional Modes

7.4.1 Output Voltage

The LM1085 adjustable version develops a 1.25V reference voltage, (V_{REF}), between the output and the adjust terminal. As shown in Figure 13, this voltage is applied across resistor R1 to generate a constant current I1. This constant current then flows through R2. The resulting voltage drop across R2 adds to the reference voltage to sets the desired output voltage.

The current I_{ADJ} from the adjustment terminal introduces an output error. But since it is small (120uA max), it becomes negligible when R1 is in the 100 Ω range.

For fixed voltage devices, R1 and R2 are integrated inside the devices.

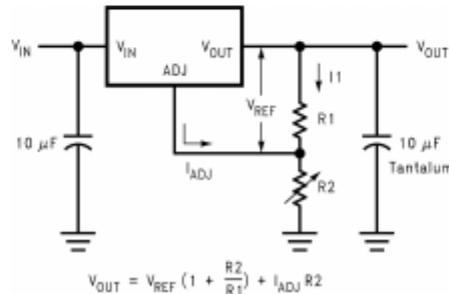


Figure 13. Basic Adjustable Regulator

7.4.2 Stability Consideration

Stability consideration primarily concerns the phase response of the feedback loop. In order for stable operation, the loop must maintain negative feedback. The LM1085 requires a certain amount series resistance with capacitive loads. This series resistance introduces a zero within the loop to increase phase margin and thus increase stability. The equivalent series resistance (ESR) of solid tantalum or aluminum electrolytic capacitors is used to provide the appropriate zero (approximately 500 kHz).

Aluminum electrolytics are less expensive than tantalums, but their ESR varies exponentially at cold temperatures; therefore requiring close examination when choosing the desired transient response over temperature. Tantalums are a convenient choice because their ESR varies less than 2:1 over temperature.

The recommended load/decoupling capacitance is a 10uF tantalum or a 50uF aluminum. These values will assure stability for the majority of applications.

The adjustable versions allow an additional capacitor to be used at the ADJ pin to increase ripple rejection. If this is done the output capacitor should be increased to 22 uF for tantalum or to 150 uF for aluminum.

Capacitors other than tantalum or aluminum can be used at the adjust pin and the input pin. A 10uF capacitor is a reasonable value at the input. See [Ripple Rejection](#) section regarding the value for the adjust pin capacitor.

Device Functional Modes (continued)

It is desirable to have large output capacitance for applications that entail large changes in load current (microprocessors for example). The higher the capacitance, the larger the available charge per demand. It is also desirable to provide low ESR to reduce the change in output voltage:

$$V = \Delta I \times ESR \quad (2)$$

It is common practice to use several tantalum and ceramic capacitors in parallel to reduce this change in the output voltage by reducing the overall ESR.

Output capacitance can be increased indefinitely to improve transient response and stability.

7.4.3 Protection Diodes

Under normal operation, the LM1085 regulator does not need any protection diode. With the adjustable device, the internal resistance between the adjustment and output terminals limits the current. No diode is needed to divert the current around the regulator even with a capacitor on the adjustment terminal. The adjust pin can take a transient signal of ± 25 V with respect to the output voltage without damaging the device.

When an output capacitor is connected to a regulator and the input is shorted, the output capacitor will discharge into the output of the regulator. The discharge current depends on the value of the capacitor, the output voltage of the regulator, and rate of decrease of V_{IN} . In the LM1085 regulator, the internal diode between the output and input pins can withstand microsecond surge currents of 10 A to 20 A. With an extremely large output capacitor ($\geq 1000 \mu\text{f}$), and with input instantaneously shorted to ground, the regulator could be damaged. In this case, an external diode is recommended between the output and input pins to protect the regulator, shown in Figure 14.

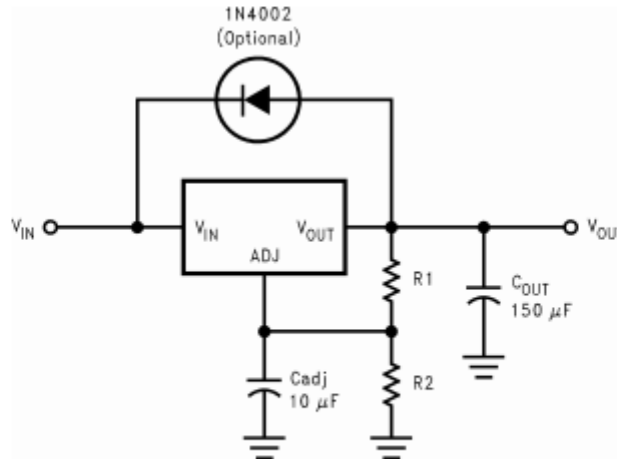


Figure 14. Regulator With Protection Diode

8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

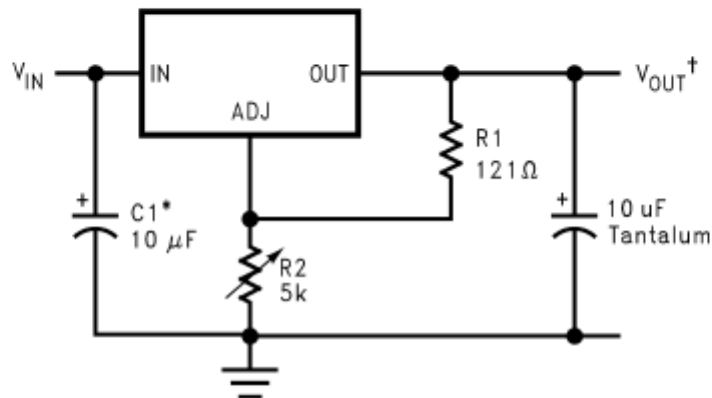
8.1 Application Information

The LM1085 is versatile in its applications, including uses in programmable output regulation and local on-card regulation. Or, by connecting a fixed resistor between the ADJUST and OUTPUT terminals, the LM1085 can function as a precision current regulator. An optional output capacitor can be added to improve transient response. The ADJUST terminal can be bypassed to achieve very high ripple-rejection ratios, which are difficult to achieve with standard three-terminal regulators. Please note, in the following applications, if ADJ is mentioned, it makes use of the adjustable version of the part, however, if GND is mentioned, it is the fixed voltage version of the part.

8.2 Typical Applications

8.2.1 1.2-V to 15-V Adjustable Regulator

This part can be used as a simple low drop out regulator to enable a variety of output voltages needed for demanding applications. By using an adjustable R2 resistor a variety of output voltages can be made possible as shown in Figure 15 based on the LM1085-ADJ.



*NEEDED IF DEVICE IS FAR FROM FILTER CAPACITORS

$$†V_{OUT} = 1.25V \left(1 + \frac{R2}{R1}\right)$$

Figure 15. 1.2-V to 15-V Adjustable Regulator

8.2.1.1 Design Requirements

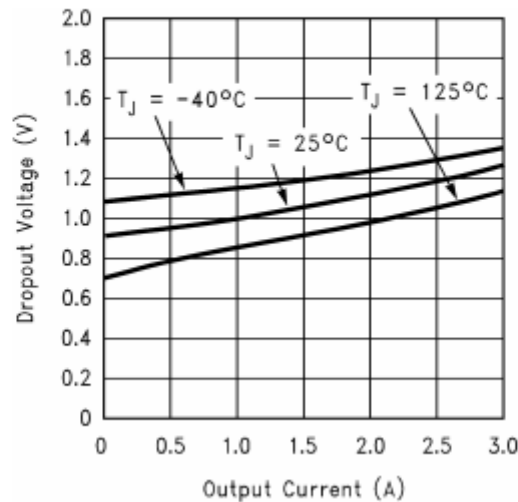
The device component count is very minimal, employing two resistors as part of a voltage divider circuit and an output capacitor for load regulation.

8.2.1.2 Detailed Design Procedure

The voltage divider for this part is set based on the equation in Figure 15, where R1 is the upper feedback resistor R2 is the lower feedback resistor.

Typical Applications (continued)

8.2.1.3 Application Curve



8.2.2 Adjustable at 5 V

The application shown in Figure 16 outlines a simple 5 V output application made possible by the LM1085-ADJ. This application can provide 3 A at high efficiencies and very low drop-out.

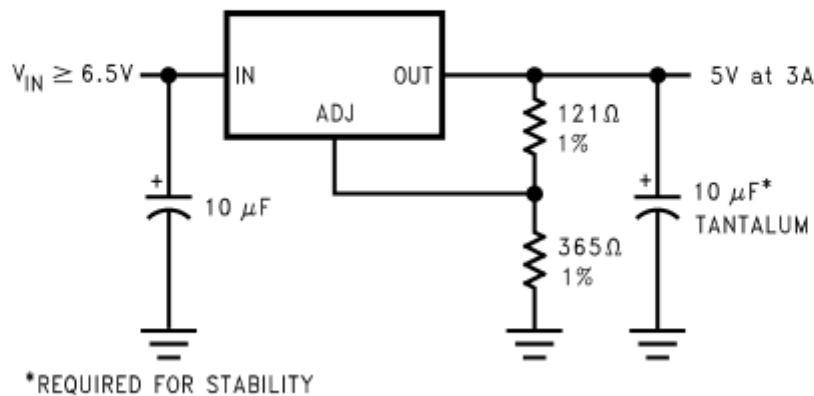


Figure 16. Adjustable @ 5V

Typical Applications (continued)

8.2.3 5-V Regulator with Shutdown

A variation of the 5 V output regulator application with shutdown control is shown in Figure 17 based on the LM1085-ADJ. It uses a simple NPN transistor on the ADJ pin to block or sink the current on the ADJ pin. If the TTL logic is pulled high, the NPN transistor is activated and the part is disabled, outputting approximately 1.25 V. If the TTL logic is pulled low, the NPN transistor is unbiased and the regulator functions normally.

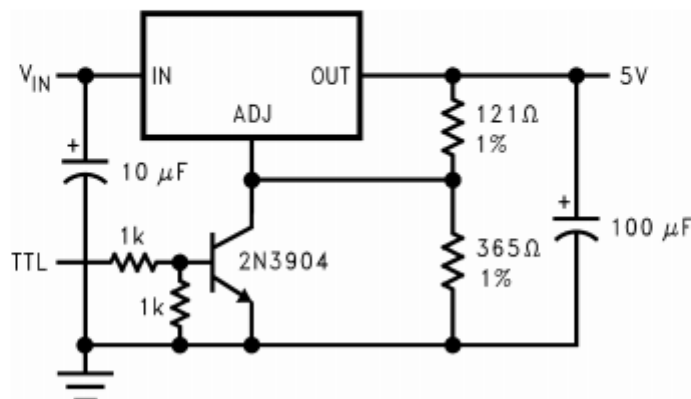


Figure 17. 5-V Regulator with Shutdown

8.2.4 Battery Charger

The LM1085-ADJ can be used as a battery charger to regulate the charging current required by the battery bank as shown in Figure 18. In this application the LM1085 acts as a constant voltage, constant current part by sensing the voltage potential across the battery and compensating it to the current voltage. To maintain this voltage, the regulator delivers the maximum charging current required to charge the battery. As the battery approaches the fully charged state, the potential drop across the sense resistor, R_S , reduces and the regulator throttles back the current to maintain the float voltage of the battery.

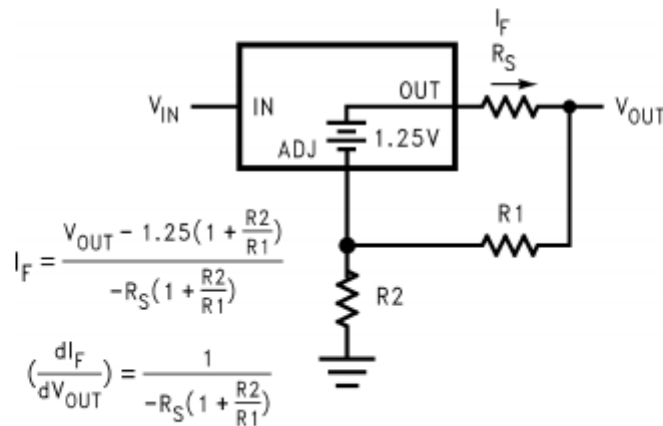
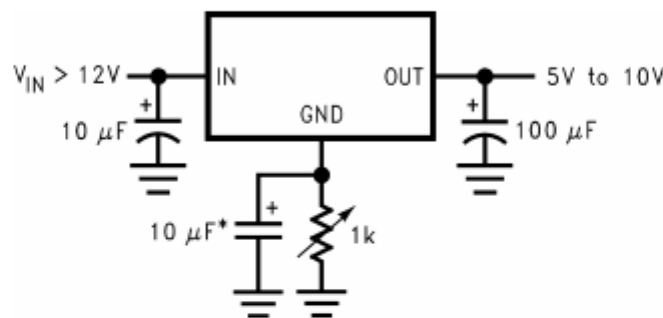


Figure 18. Battery Charger

Typical Applications (continued)

8.2.5 Adjustable Fixed Regulator

A simple adjustable, fixed range output regulator can be made possible by placing a variable resistor on the ground of the device as shown in Figure 19 based on the fixed output voltage LM1085-5.0. The GND pin has a small quiescent current of 5 mA typical. Increasing the resistance on the GND pin increases the voltage potential across the resistor. This potential is then mirrored on to the output to increase the total output voltage by the potential drop across the GND resistor.



*OPTIONAL IMPROVES RIPPLE REJECTION

Figure 19. Adjustable Fixed Regulator

8.2.6 Regulator with Reference

A fixed output voltage version of the LM1085-5.0 can be employed to provide an output rail and a reference rail at the same time as shown in Figure 20. This simple application makes use of a reference diode, the LM136-5, to regulate the GND voltage to a fixed 5 V based on the quiescent current generated by the GND pin. This voltage is then added onto the output to generate a total of 10 V out.

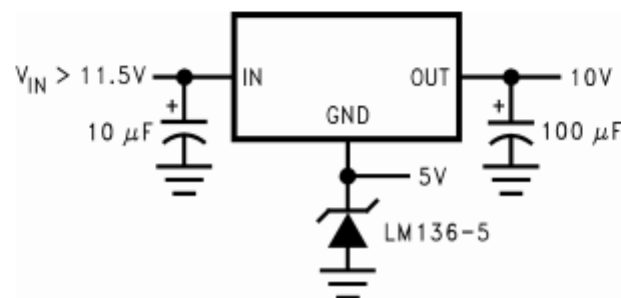


Figure 20. Regulator With Reference

8.2.7 High Current Lamp Driver Protection

A simple constant current source with protection can be designed by controlling the impedance between the lamp and ground. The LM1085-ADJ shown in Figure 21 makes use of an external TTL or CMOS input to drive the NPN transistor. This pulls the output of the regulator to a few tenths of a volt and puts the part into current limit. Releasing the logic will reduce the current flow across the lamp into the normal operating current thereby protecting the lamp during startup.

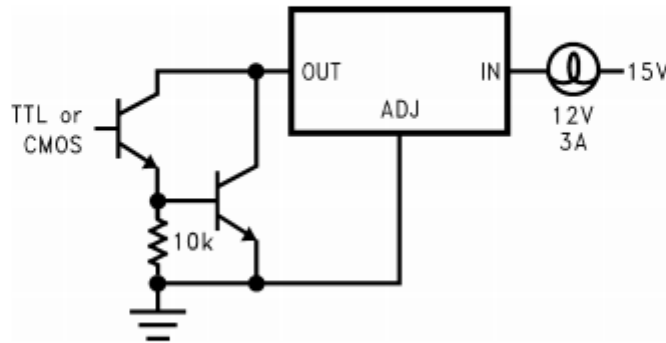


Figure 21. High Current Lamp Driver Protection

8.2.8 Battery Backup Regulated Supply

A regulated battery backup supply can be generated by using two fixed output voltage versions of the part as shown in Figure 22. The top regulator supplies the Line voltage during normal operation, however when the input is not available, the second regulator derives power from the battery backup and regulates it to 5 V based on the LM1085-5.0. The diodes prevent the rails from back feeding into the supply and batteries.

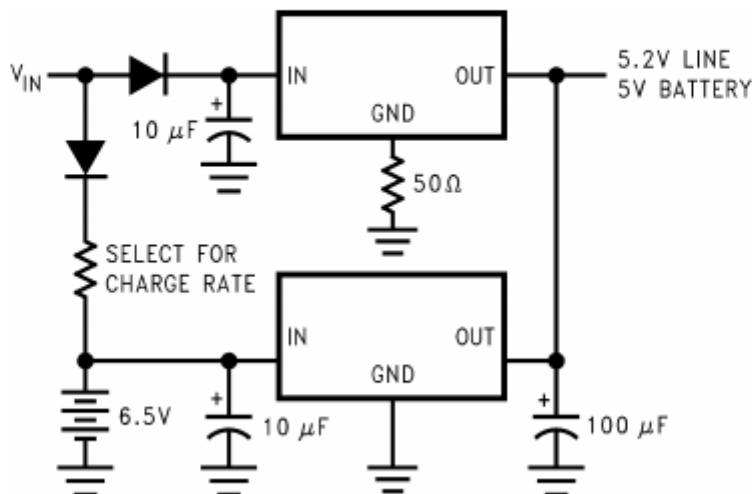
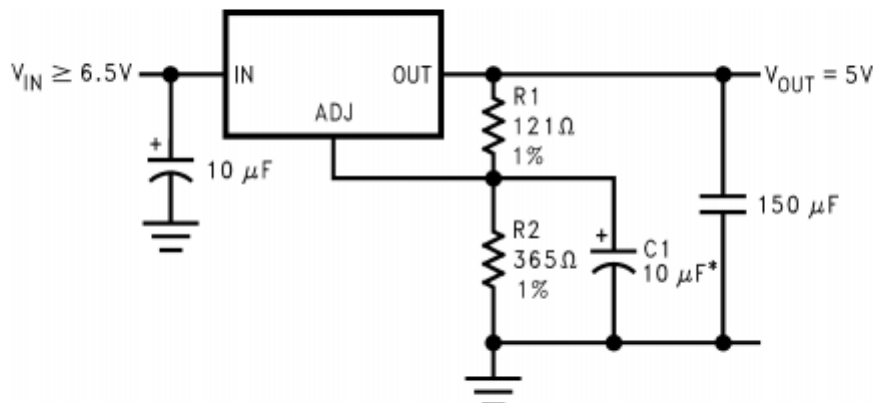


Figure 22. Battery Backup Regulated Supply

8.2.9 Ripple Rejection Enhancement

A very simple ripple rejection circuit is shown in Figure 23 using the LM1085-ADJ. The capacitor C1 smooths out the ripple on the output by cleaning up the feedback path and preventing excess noise from feeding back into the regulator. Please remember X_{C1} should be approximately equal to R1 at the ripple frequency.



*C1 IMPROVES RIPPLE REJECTION.
 X_C SHOULD BE \approx R1 AT RIPPLE FREQUENCY

Figure 23. Ripple Rejection Enhancement

8.2.10 Automatic Light Control

A common street light control or automatic light control circuit is designed in Figure 24 based on the LM1085-ADJ. The photo transistor conducts in the presence of light and grounds the ADJ pin preventing the lamp from turning on. However, in the absence of light, the LM1085 regulates the voltage to 1.25V between OUT and ADJ, ensuring the lamp remains on.

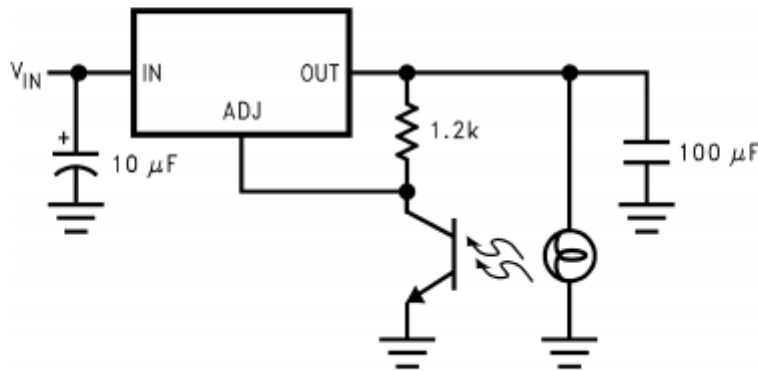


Figure 24. Automatic Light Control

8.2.11 Generating Negative Supply Voltage

A quick inverting output rail or negative output rail is shown in Figure 25 using the LM1085 fixed output part. By tying the output to GND, the GND node is at a relatively more negative potential than the output. This is then interfaced to the negative application such as an operational amplifier or any other rail needing negative voltage.

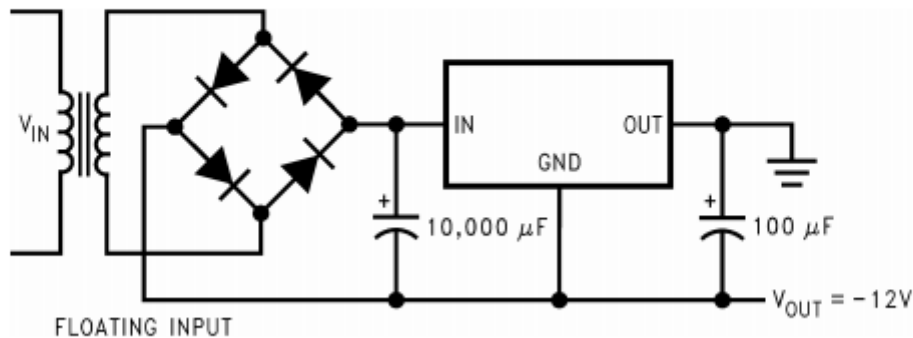


Figure 25. Generating Negative Supply Voltage

8.2.12 Remote Sensing

Remote sensing is a method of compensating the output voltage to a very precise degree by sensing the output and feeding it back through the feedback. The circuit implementing this is shown in Figure 26 using the LM1085-ADJ. The output of the regulator is fed into a voltage follower to avoid any loading effects and the output of the op-amp is injected into the top of the feedback resistor network. This has the effect of modulating the voltage to a precise degree without additional loading on the output.

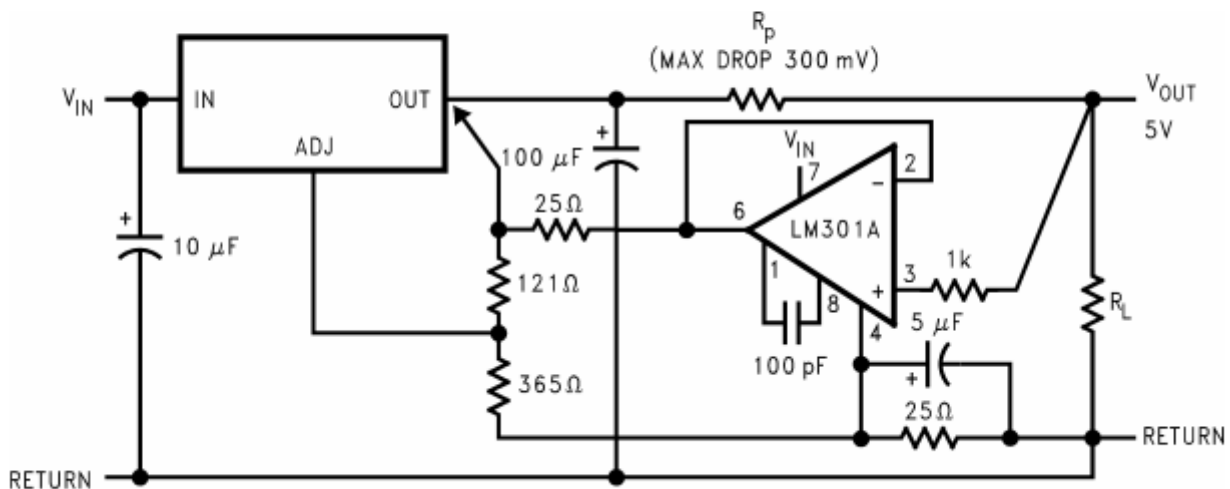


Figure 26. Remote Sensing

9 Power Supply Recommendations

The linear regulator input supply should be well regulated and kept at a voltage level such that the maximum input to output voltage differential allowed by the device is not exceeded. The minimum dropout voltage ($V_{IN} - V_{OUT}$) should be met with extra headroom when possible in order to keep the output well regulated. A 10 μF or higher capacitor should be placed at the input to bypass noise.

10 Layout

10.1 Layout Guidelines

For the best overall performance, some layout guidelines should be followed. Place all circuit components on the same side of the circuit board and as near as practical to the respective linear regulator pins connections. Traces should be kept short and wide to reduce the amount of parasitic elements into the system. The actual width and thickness of traces will depend on the current carrying capability and heat dissipation required by the end system. An array of plated vias can be placed on the pad area underneath the TAB to conduct heat to any inner plane areas or to a bottom-side copper plane.

10.2 Layout Example

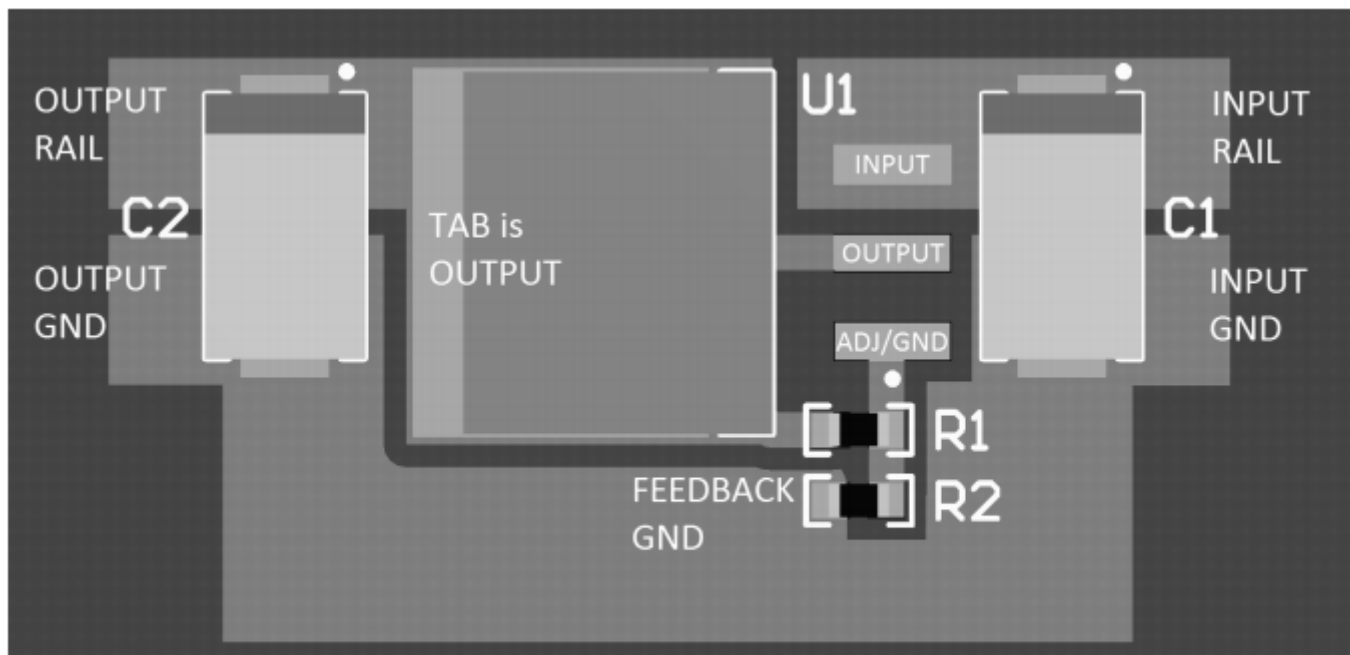


Figure 27. Layout Example

10.3 Thermal Considerations

ICs heats up when in operation, and power consumption is one factor in how hot it gets. The other factor is how well the heat is dissipated. Heat dissipation is predictable by knowing the thermal resistance between the IC and ambient (θ_{JA}). Thermal resistance has units of temperature per power (C/W). The higher the thermal resistance, the hotter the IC.

The LM1085 specifies the thermal resistance for each package as junction to case (θ_{JC}). In order to get the total resistance to ambient (θ_{JA}), two other thermal resistance must be added, one for case to heat-sink (θ_{CH}) and one for heatsink to ambient (θ_{HA}). The junction temperature can be predicted as follows:

$$T_J = T_A + P_D (\theta_{JC} + \theta_{CH} + \theta_{HA}) = T_A + P_D \theta_{JA} \quad (3)$$

T_J is junction temperature, T_A is ambient temperature, and P_D is the power consumption of the device. Device power consumption is calculated as follows:

Thermal Considerations (continued)

$$I_{IN} = I_L + I_G \quad (4)$$

$$P_D = (V_{IN} - V_{OUT}) I_L + V_{IN} I_G \quad (5)$$

Figure 28 shows the voltages and currents which are present in the circuit.

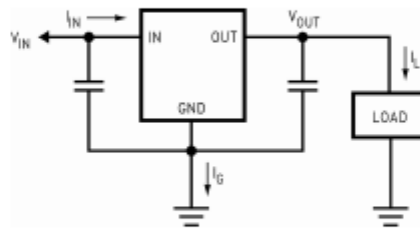


Figure 28. Power Dissipation Diagram

Once the device's power is determined, the maximum allowable ($\theta_{JA(max)}$) is calculated as:

$$\theta_{JA(max)} = T_{R(max)}/P_D = T_{J(max)} - T_{A(max)}/P_D$$

The LM1085 has different temperature specifications for two different sections of the IC: the control section and the output section. The [Thermal Information](#) table shows the junction to case thermal resistances for each of these sections, while the maximum junction temperatures ($T_{J(max)}$) for each section is listed in the [Absolute Maximum Ratings](#) section of the datasheet. $T_{J(max)}$ is 125°C for the control section, while $T_{J(max)}$ is 150°C for the output section.

$\theta_{JA(max)}$ should be calculated separately for each section as follows:

$$\theta_{JA(max, CONTROL SECTION)} = (125^\circ\text{C} - T_{A(max)})/P_D \quad (6)$$

$$\theta_{JA(max, OUTPUT SECTION)} = (150^\circ\text{C} - T_{A(max)})/P_D \quad (7)$$

The required heat sink is determined by calculating its required thermal resistance ($\theta_{HA(max)}$).

$$\theta_{HA(max)} = \theta_{JA(max)} - (\theta_{JC} + \theta_{CH}) \quad (8)$$

($\theta_{HA(max)}$) should also be calculated twice as follows:

$$(\theta_{HA(max)}) = \theta_{JA(max, CONTROL SECTION)} - (\theta_{JC(CONTROL SECTION)} + \theta_{CH}) \quad (9)$$

$$(\theta_{HA(max)}) = \theta_{JA(max, OUTPUT SECTION)} - (\theta_{JC(OUTPUT SECTION)} + \theta_{CH}) \quad (10)$$

If thermal compound is used, θ_{CH} can be estimated at 0.2 C/W. If the case is soldered to the heat sink, then a θ_{CH} can be estimated as 0 C/W.

After, $\theta_{HA(max)}$ is calculated for each section, choose the lower of the two $\theta_{HA(max)}$ values to determine the appropriate heat sink.

If PC board copper is going to be used as a heat sink, then Figure 29 can be used to determine the appropriate area (size) of copper foil required.

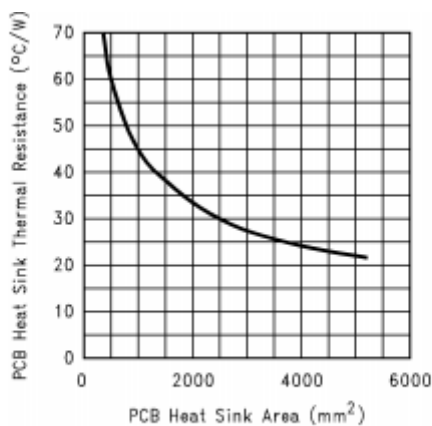


Figure 29. Heat Sink Thermal Resistance vs Area